

Features

- 2A Output Current
- Wide 4.5V to 23V Operating Input Range
- Integrated Power MOSFET Switches
- Output Adjustable from 0.925V to 18V
- Up to 96% Efficiency
- Programmable Soft-Start
- Stable with Low ESR Ceramic Output Capacitors
- Fixed 400KHZ Frequency
- Cycle-by-Cycle Over Current Protection
- Input Under Voltage Lockout
- Package : SOP-8L

Applications

- Distributed Power Systems
- Networking Systems
- FPGA, DSP, ASIC Power Supplies

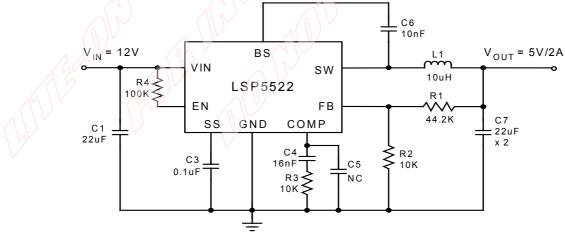
Typical Application Circuit

General Description

The LSP5522 is a monolithic synchronous buck regulator. The device integrates $150m\Omega$ MOSFETS that provide 2A continuous load current over a wide operating input voltage of 4.5V to 23V. Current mode control provides fast transient response and cycle-by-cycle current limit.

An adjustable soft-start prevents inrush current at turn on. In shutdown mode, the supply current drops below 1uA.

- Green Electronics/ Appliances
- Notebook Computers



shows a sample LSP5522 application circuit generating 5V/2A output

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Ordering Information

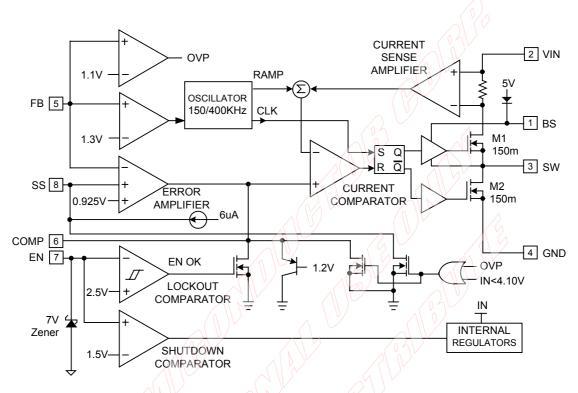
Package : Output Voltage : Packing : S : SOP-8L Blank : ADJ A : Tape & Reel Device Package Code Package Tape & Reel LSP5522SA S SOP-8L 2500 A Pin Assignments SOP-8L SOP-8L COMP NN 2 9 8 8 Pin Assignments SOP-8L 7 EN NN 2 5 FB Pin Descriptions FB FB		LSP552	2 <u>X X X</u>		
Device Package Code Package Quantity Part Number Suffix LSP5522SA S SOP-8L 2500 A Pin Assignments SOP-8L (TOP View) SOP-8L 8 SOP-8L 7 EN BS<1 0 8 SS VIN<2 7 EN SW<3 6 COMP GND 5 FB					Reel
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LSP5522SA S SOP-8L 2500 A Pin Assignments SOP-8L (TOP View) SOP-8L (TOP View) SOP-8L (TOP View) Es 1 0 8 SS 7 EN 6 COMP 6 COMP 5 FB 5 FB 6 COMP 6 COMP<	Device	Package Code	Package		Part Number
BS 1 VIN 2 SW 3 GND 4 SW 5 FB	LSP5522SA	S	SOP-8L	2500	
		BS VIN SW GND	(TOP View) 1 0 2 7 1 3 6	EN	

Pin Number	Name	Description
1	BS	Bootstrap. This pin acts as the positive rail for the high-side switch's gate driver. Connect a 0.1uF capacitor between BS and SW.
2	VIN	Input Supply. Bypass this pin to G with a low ESR capacitor. See Input Capacitor in the Application Information section.
3	ŚW	Switch Output. Connect this pin to the switching end of the inductor.
4	GND	Ground.
5	FB	Feedback Input. The voltage at this pin is regulated to 0.925V. Connect to the resistor divider between output and ground to set output voltage.
6	COMP	Compensation Pin. See Stability Compensation in the Application Information section.
7	EN	Enable Input. When higher than 2.5V, this pin turns the IC on. When lower than 1.3V, this pin turns the IC off. Output voltage is discharged when the IC is off. This pin should not be left open.
8	SS	Soft-Start Control Input. SS controls the soft-start period. Connect a capacitor from SS to GND to set the soft-start period. A 0.1uF capacitor sets the soft-start period to 15ms. To disable the soft-start feature, leave SS unconnected.





Block Diagram



Absolute Maximum Ratings

Parameter	Value	Unit
Input Supply Voltage	-0.3 to 27	V
SW Voltage	-1 to V _{IN} + 0.3	V
BS Voltage	V_{SW} – 0.3 to V_{SW} + 6	V
EN, FB, COMP Voltage	-0.3 to 6	V
Continuous SW Current	Internally limited	A
Junction to Ambient Thermal Resistance (θ_{JA})	105	°C/W
(Test on Approximately 3 in ² Copper Area 1oz copper FR4 board)	105	0/10
Junction to Ambient Case Resistance (θ_{Jc})	20	°C/W
SOP-8L Power Dissipation	0.76	W
Maximum Junction Temperature	150	°C
Storage Temperature Range	-65 to 150	°C

(Note: Exceeding these limits may damage the device. Exposure to absolute maximum rating conditions for long periods may affect device reliability.)

Recommended Operating Conditions

Parameter	Min	Max	Unit
Input Supply Voltage	4.5	23	V
Operating Junction Temperature	-20	+125	°C





Electrical Characteristics

(V_{IN} = 12V, T_A = 25°C unless otherwise specified.)

V _{FB}		Min	Тур	Max	Unit
■ FB	4.5V ≤ VIN ≤ 23V	0.900	0.925	0.950	V
		/	1.1		V
			150		mΩ
	(ph)	1	150		mΩ
	$V_{EN} = 0V, V_{SW} = 0V$		0.1	10	uA
			3.5	4.0	Α
G _{COMP}			4		A/V
G _{EA}	$\Delta I_{COMP} = \pm 10 uA$	~	800		uA/V
AVEA			480		V/V
f _{SW}		350	400	470	KHz
~	V _{FB} = 0		150		KHz
D _{MAX}	V _{FB} = 0,8V			90	%
		40	220		nS
	V _{EN} Rising)/1.1	1.4	2	V
	A B	r	100		mV
		2.2	2.5	2.7	V
			150		mV
0	V _{EN} = 0		0.3	3.0	uA
	$V_{EN} = 3V, V_{FB} = 1.0V$		1.4	1.5	mA
UVLO	V _{EN} Rising	3.80	4.05	4.40	V
$\langle V \rangle$	$\land \lor$		100		mV
\vee	V _{SS} = 0V		6		uA
	C _{SS} = 0.1uF		15		mS
{	Hysteresis = 10°C		150		°C
	G _{EA} A _{VEA} f _{SW} D _{MAX}	G_{COMP} G_{EA} $\Delta I_{COMP} = \pm 10 \mu A$ A_{VEA} f_{SW} f_{SW} $V_{FB} = 0$ D_{MAX} $V_{FB} = 0.8 V$ V_{EN} Rising $V_{EN} = 0$ $V_{EN} = 3V, V_{FB} = 1.0V$ V_{EN} Rising $V_{SS} = 0V$		$\begin{tabular}{ c c c c c c c } \hline & & & & & & & & & & & & & & & & & & $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $





Application Description

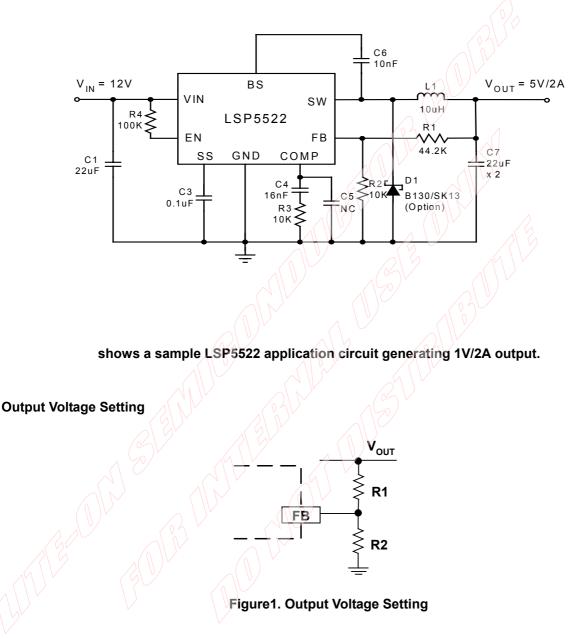


Figure 1 shows the connections for setting the output voltage. Select the proper ratio of the two feedback resistors R_{FB1} and R_{FB2} based on the output voltage. Typically, use $R_{FB2} \approx 10 K\Omega$ and determine R_{FB1} from the following equation:



LSP5522

2A Synchronous Step Down DC/DC Converter

Application Description (Continued)

$R_{FB1} = R_{FB2}$	$\left(\frac{V_{OUT}}{0.925V}-1\right)$	(1)
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ble1 - Recommended Resistance Values							
RFB1	RFB2						
1.0 ΚΩ	12 KΩ						
3.0 ΚΩ	10 KΩ						
9.53 ΚΩ	10 KΩ						
16.9 ΚΩ	10 KΩ						
26.1 ΚΩ	10 KΩ						
44.2 KΩ	10 KΩ						
121 KΩ	10 KΩ						
	RFB1 1.0 KΩ 3.0 KΩ 9.53 KΩ 16.9 KΩ 26.1 KΩ 44.2 KΩ						

Inductor Selection

The inductor maintains a continuous current to the output load. This inductor current has a ripple that is dependent on the inductance value: higher inductance reduces the peak-to-peak ripple current. The trade off for high inductance value is the increase in inductor core size and series resistance, and the reduction in current handling capability. In general, select an inductance value L based on the ripple current requirement:

 $L = \frac{V_{OUT} \bullet (V_{IN} - V_{OUT})}{V_{IN} f_{SW} I_{OUTMAX} K_{RIPPLE}}$ (2)

where V_{IN} is the input voltage, V_{OUT} is the output voltage, f_{SW} is the switching frequency, I_{OUTMAX} is the maximum output current, and K_{RIPPLE} is the ripple factor. Typically, choose K_{RIPPLE} = 30% to correspond to the peak-to-peak ripple current being 30% of the maximum output current.

With this inductor value, the peak inductor current is $I_{OUT} \cdot (1 + K_{RIPPLE} / 2)$. Make sure that this peak inductor current is less that the 3A current limit. Finally, select the inductor core size so that it does not saturate at 3A. Typical inductor values for various output voltages are shown in Table 1.

			. \ \\ '					
001	1.0V		N 2					9V
	10uH	10uH	10uH	10uH	10uH	10uH	10uH	33uH

Table 1. Typical Inductor Values

Input Capacitor

The input capacitor needs to be carefully selected to maintain sufficiently low ripple at the supply input of the converter. A low ESR capacitor is highly recommended. Since large current flows in and out of this capacitor during switching, its ESR also affects efficiency.

The input capacitance needs to be higher than 10uF. The best choice is the ceramic type; however, low ESR tantalum or electrolytic types may also be used provided that the RMS ripple current rating is higher than 50% of the output current. The input capacitor should be placed close to the VIN and GND pins of the IC, with the shortest traces possible. In the case of tantalum or electrolytic types, they can be further away if a small parallel 0.1uF ceramic capacitor is placed right next to the IC.



Application Description (Continued)

Output Capacitor

The output capacitor also needs to have low ESR to keep low output voltage ripple. The output ripple voltage is:

 $V_{RIPPLE} = I_{OUTMAX} K_{RIPPLE} R_{ESR} + \frac{V_{IN}}{28 \bullet f_{SW}^2 L C_{OUT}}$ (3)

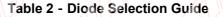
where I_{OUTMAX} is the maximum output current, K_{RIPPLE} is the ripple factor, R_{ESR} is the ESR of the output capacitor, f_{SW} is the switching frequency, L is the inductor value, and C_{OUT} is the output capacitance. In the case of ceramic output capacitors, R_{ESR} is very small and does not contribute to the ripple. Therefore, a lower capacitance value can be used for ceramic capacitors. In the case of tantalum or electrolytic capacitors, the ripple is dominated by R_{ESR} multiplied by the ripple current. In that case, the output capacitor is chosen to have sufficiently low ESR.

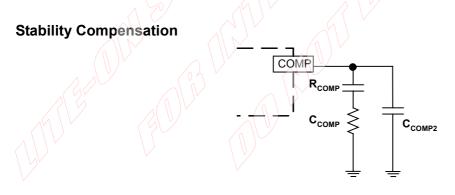
For ceramic output capacitors, typically choose a capacitance of about 22 μ F. For tantalum or electrolytic capacitors, choose a capacitor with less than 50m Ω ESR.

Optional Schottky Diode

During the transition between high-side switch and low-side switch, the body diode of the low side power MOSFET conducts the inductor current. The forward voltage of this body diode is high. An optional Schottky diode may be paralleled between the SW pin and GND pin to improve overall efficiency. Table 2 lists example Schottky diodes and their Manufacturers.

Part Number	Voltage/Current Rating	Vendor
B130	30V, 1A	Lite-on semiconductor corp.
SK13	30V, 1A	Lite-on semiconductor corp.





C_{COMP2} is needed only for high ESR output capacitor

Figure 2. Stability Compensation

The feedback loop of the IC is stabilized by the components at the COMP pin, as shown in Figure 2. The DC loop gain of the system is determined by the following equation:

$$A_{VDC} = \frac{0.925}{I_{OUT}} \vee_{A_{VEA}} G_{COMP}$$
 (4)

The dominant pole P1 is due to C_{COMP} :



Application Description (Continued)

$$f_{P1} = \frac{G_{EA}}{2\pi A_{VEA} C_{COMP}}$$
(5)

The second pole P2 is the output pole:

$$f_{P2} = \frac{I_{OUT}}{2\pi V_{OUT} C_{OUT}}$$
(6)

The first zero Z1 is due to R_{COMP} and C_{COMP} :

$$f_{Z1} = \frac{1}{2\pi R_{COMP} C_{COMP}}$$
(7)

And finally, the third pole is due to R_{COMP} and C_{COMP2} (if C_{COMP2} is used):

$$f_{P3} = \frac{1}{2\pi R_{COMP} C_{COMP2}}$$
(8)

The following steps should be used to compensate the IC:

STEP1. Set the crossover frequency at 1/10 of the switching frequency via R_{COMP}:

$$R_{COMP} = \frac{2\pi V_{OUT} C_{OUT} f_{SW}}{10G_{EA}G_{COMP} \bullet 0.925V}$$
(9)

but suggest R_{COMP} to $10K\Omega$ maximum.

STEP2. Set the zero fZ1 at 1/4 of the crossover frequency. If R_{COMP} is less than 10K Ω , the equation for C_{COMP} is:

$$C_{COMP} = \frac{1.8 \times 10^{-5}}{R_{COMP}}$$
 (F) (10)

If R_{COMP} is limited to 10K Ω , then the actual crossover frequency is 10/ ($V_{OUT}C_{OUT}$). Therefore: $C_{COMP} = 1.2 \times 10^{-5} V_{OUT}C_{OUT}$ (F) (11)

STEP3. If the output capacitor's ESR is high enough to cause a zero at lower than 4 times the crossover frequency, an additional compensation capacitor C_{COMP2} is required. The condition for using C_{COMP2} is:

$$R_{ESRCOUT} \ge Min\left(\frac{1.1 \times 10^{-6}}{C_{OUT}}, 0.012 \bullet V_{OUT}\right) \qquad (\Omega) \qquad (12)$$

And the proper value for $C_{\mbox{\scriptsize COMP2}}$ is:



Application Description (Continued)

$$C_{COMP2} = \frac{C_{OUT}R_{ESRCOUT}}{R_{COMP}}$$
(13)



Though C_{COMP2} is unnecessary when the output capacitor has sufficiently low ESR, a small value C_{COMP2} such as 100pF may improve stability against PCB layout parasitic effects.

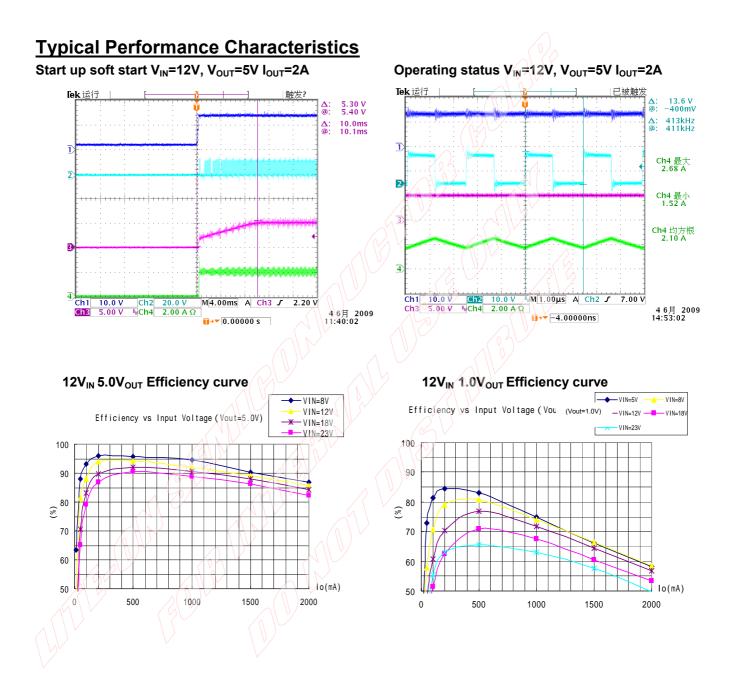
Table 3 shows some calculated results based on the compensation method above.

V _{OUT}	C _{OUT}	R _{COMP}	C _{COMP}	C _{COMP2}
0.925 V	22uF(10 mΩ ESR)	1.8 KΩ	8.6 nF	None
2.5 V	22uF(10 mΩ ESR)	5.1 ΚΩ	3.3 nF	None
3.3 V	22uF(10 mΩ ESR)	6.8 KΩ	2.4 nE	None
5 V	22uF(10 mΩ ESR)	10 KΩ	1.6 nF	/ None
9 V	22uF(10 mΩ ESR)	18 KΩ	910 pF	None
9 V	22uF(101112)E3K)	10 KΩ	2.7 nF	None
12 V	22uF(10 mΩ ESR)	24 ΚΩ	680 pF	None
12 V	22UF(101112 ESK)	10 ΚΩ	3.9 nF	None
15.1/		30 ΚΩ	560 pF	None
15 V	22uF(10 mΩ ESR)	10 ΚΩ	4.7 nF	None
18 V	224E(10 m0 ESP)	36 KΩ	430 pF	None
10 V	22uF(10 mΩ ESR)	10 KΩ	5.6 nF	None
20 V	22uF(10 mΩ ESR)	<u>39 KΩ</u>	390 pF	None
20 V		10 ΚΩ	6.2 nF	None
0.925 V	220 uF (30 mΩ ESR)-	18 ΚΩ	820 pF	360 pF
0.925 V		/ 10 KΩ /	0 3 nF	680 pF
2.5 V	220 uF(30 mΩ ESR)	51 ΚΩ	330 pF	130 pF
2.5 V		10 KΩ	8.2 nF	680 pF
3.3 V		68 KΩ	240 pF	100 pF
3.3 V	220 uF (30 mΩ ESR)	10 KΩ	10 nF	680 pF
5 V	220 uF (30 mΩ ESR)	100 KΩ	160 pF	68 pF
5 0	220 UF (30 112 ESR)	10 KΩ	16 nF	680 pF
9 V	220 uF (30 mΩ ESR)	180 ΚΩ	91 pF	36 pF
y v	220 UF (30 III22 ESR)	10 ΚΩ	27 nF	680 pF
12λ	220 uF (30 mΩ ESR)	240 ΚΩ	68 pF	27 pF
V	220 UF (30 III22 ESR)	10 KΩ	39 nF	680 pF
15 V	220 uF (30 mΩ ESR)	300 KΩ	56 pF	22 pF
V IS V		10 KΩ	47 nF	680 pF

Table3. Typical Compensation for Different Output Voltages and Output Capacitors

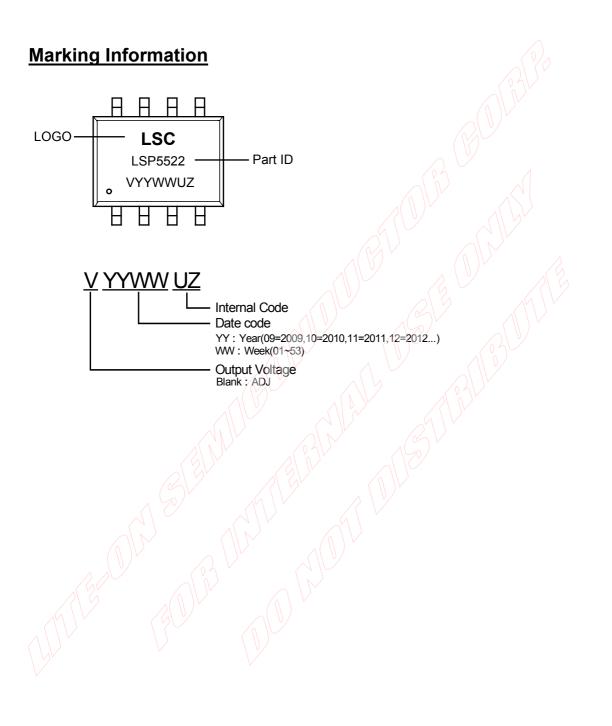






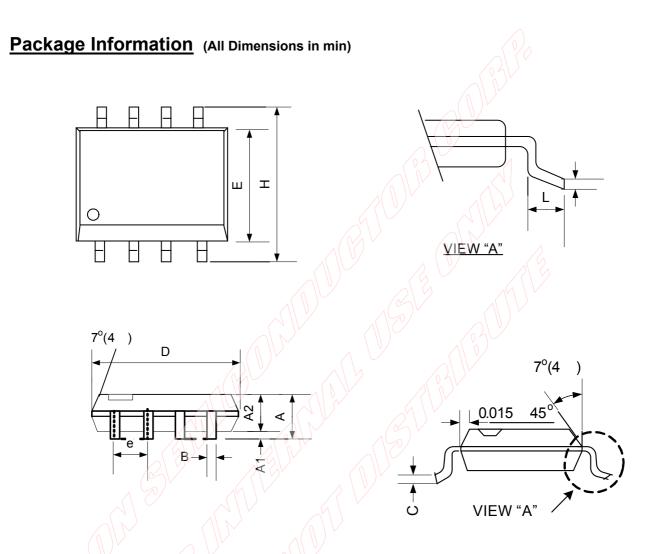












Symbol	Dimensions In Millimeters			Dimensions In Inches			
Symbol	Min	Nom	Max	Min	Nom	Max	
A	1.35	1.60	1.75	0.053	0.063	0.069	
A1	0.10		0.25	0.004		0.010	
A2	1.35	1.45	1.55	0.053	0.057	0.061	
В	0.33	0.41	0.51	0.013	0.016	0.020	
V C	0.19	0.20	0.25	0.0075	0.008	0.010	
D	4.80	4.90	5.00	0.192	0.196	0.200	
E	3.80	3.90	4.00	0.148	0.154	0.160	
е		1.27TYP.		0.050)TYP.		
Н	5.80	5.99	6.30	0.228	0.236	0.248	
Ĺ	0.38	0.71	1.27	0.015	0.028	0.050	
θ	0°		8°	0°		8°	





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